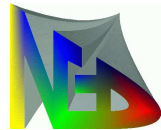


# Finite Element Methods with B-Splines

K. Höllig, J. Hörner and A. Kopf

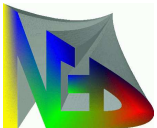
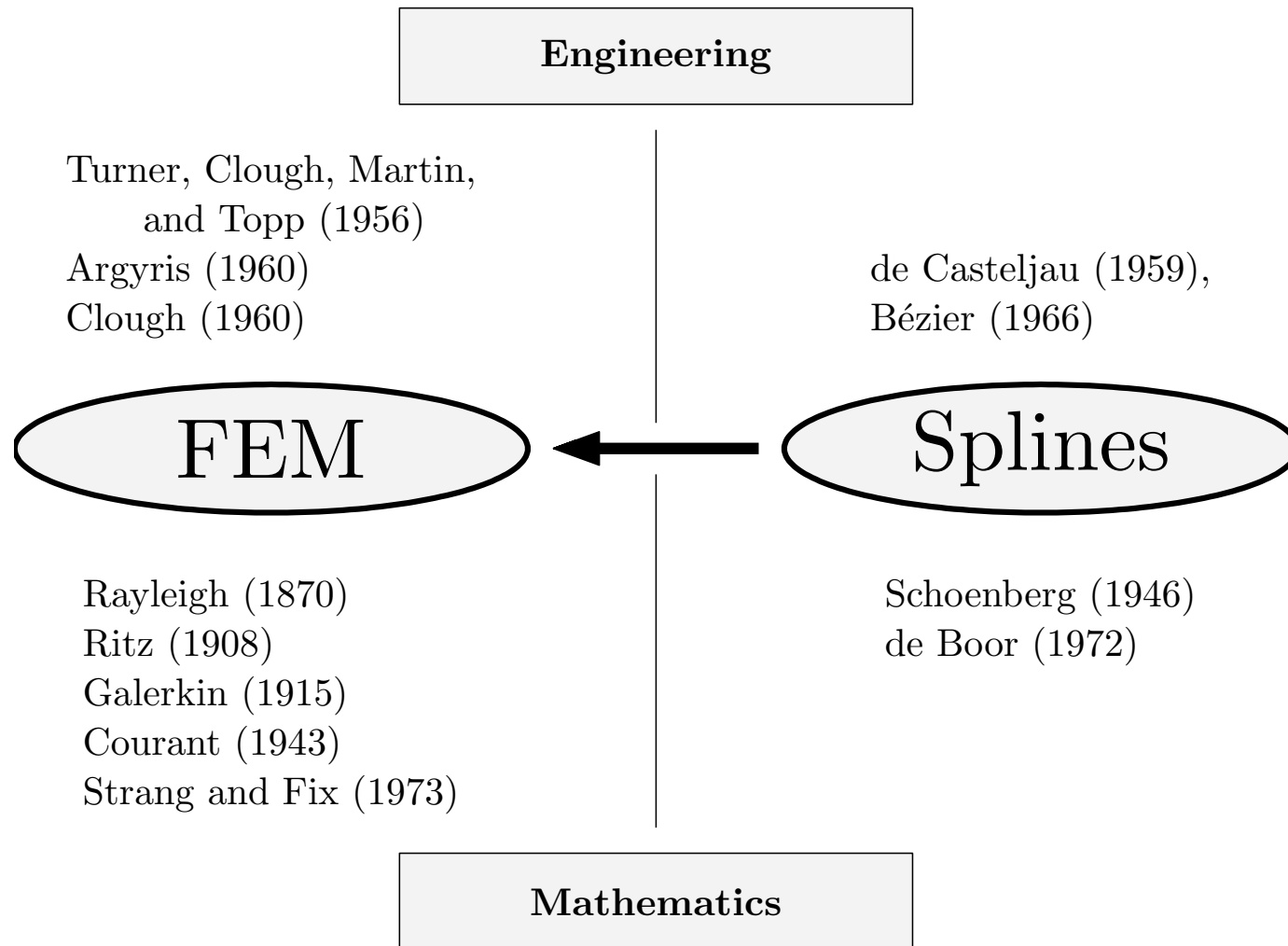


Universität Stuttgart

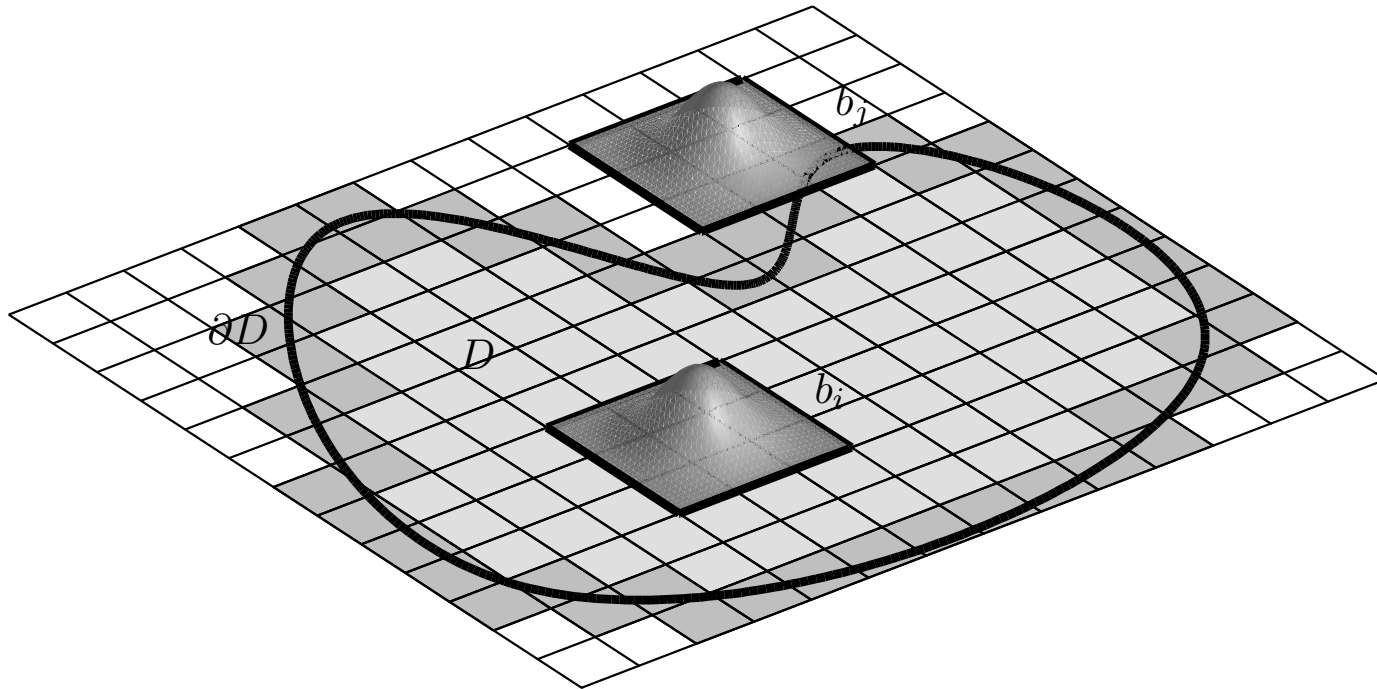
<http://www.mathematik.uni-stuttgart.de/mathA/lst2/>

<http://www.web-spline.de> (with U. Reif, J. Wipper)

# History of Finite Elements and Splines

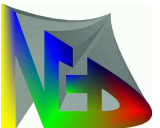


# Splines on bounded Domains

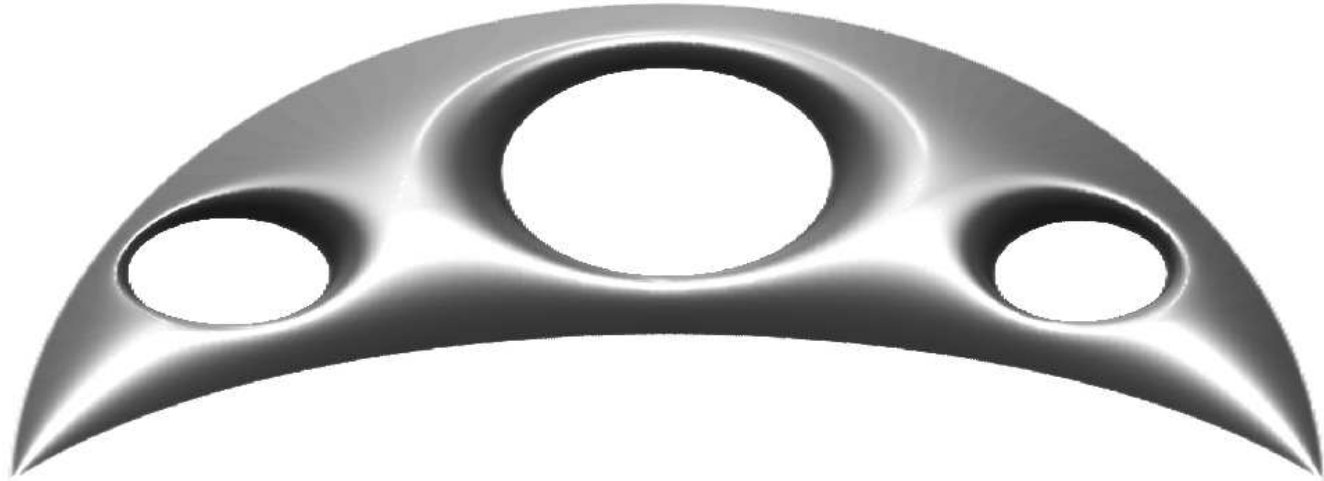


$$\mathbb{B}_h = \underset{K}{\text{span}} b_k, K = I \cup J$$

problems: boundary conditions, stability



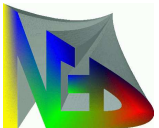
# Weight function



essential boundary conditions  $w|_{\mathcal{D}} > 0$ ,  $w|_{\partial\mathcal{D}} = 0$

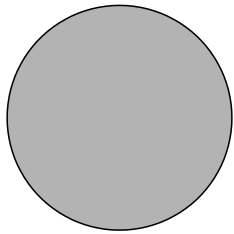
construction:

- explicit formulas
- Rvachev's Boolean expressions
- numerical distance functions

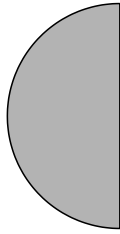


# Rvachev's R-Functions

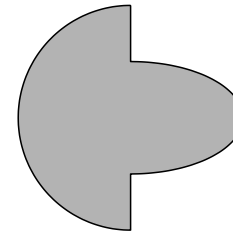
$$w_1 = 1 - x_1^2 - x_2^2$$



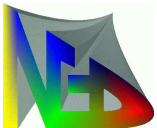
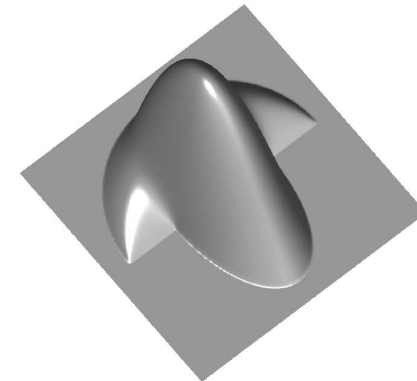
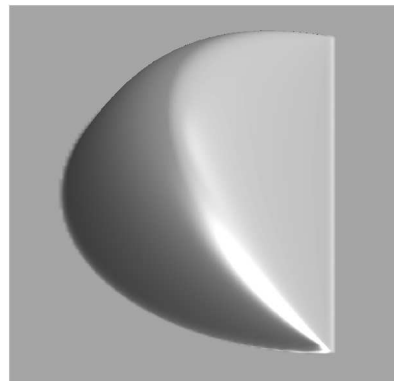
$$w_2 = -x_1$$



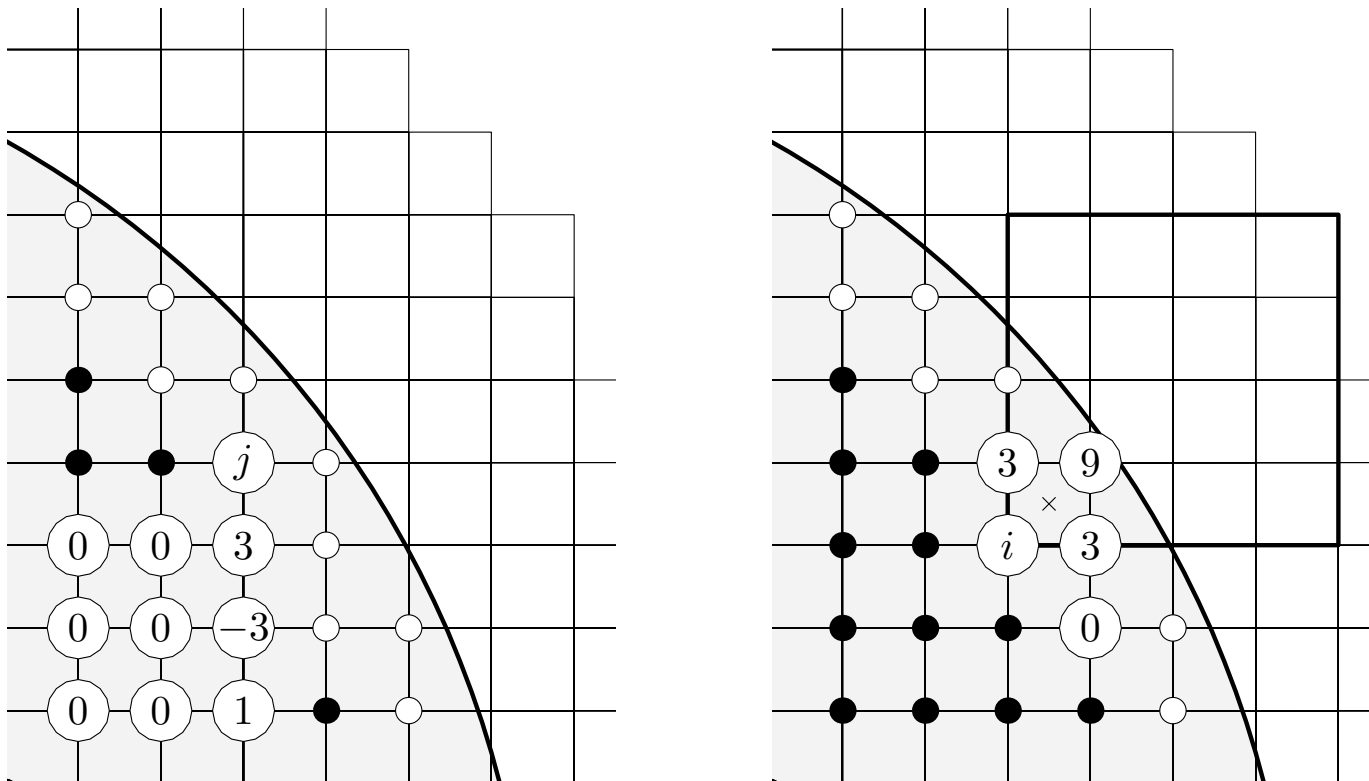
$$w_3 = 1 - x_1^2 - 4x_2^2$$



$$w_n = w_1 + w_2 - \sqrt{w_1^2 + w_2^2} \quad w_u = w_n + w_3 + \sqrt{w_n^2 + w_3^2}$$



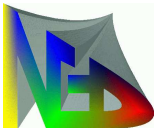
# Extension



$I(j)$  : nearest  $(n + 1)^m$ -array of inner indices

$e_{i,j}$  : value at  $j$  of the Lagrange-polynomial to  $i$

$J(i)$  : complementary sets ( $i \in I(j) \Leftrightarrow j \in J(i)$ )



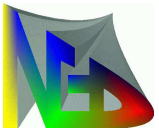
# Weighted-Extended-B-Splines

(with U. Reif and J. Wipperfurth)

$$B_i = \frac{w}{w(x_i)} \left( b_i + \sum_{j \in J(i)} e_{i,j} b_j \right)$$

properties:

- local support:  $e_{i,j} = 0$  for  $\|i - j\| \gtrsim 1$
- stability:  $\|\sum c_i B_i\|_0 \asymp \|C\|$
- approximation order:  $\|u - P_h u\|_\ell \lesssim h^{n+1-\ell} \|u\|_{n+1}$



# Ritz Galerkin Approximation

$H$  : Hilbert space, incorporating homogeneous boundary conditions

$a$  : elliptic bilinear form

$\lambda$  : linear functional

weak solution:

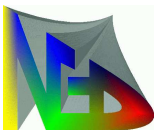
$$a(u, v) = \lambda(v), v \in H$$

finite element approximation:

$$a(u_h, B_i) = \lambda(B_i), i \in I$$

error estimate:

$$\|u - u_h\|_H \lesssim \inf_C \left\| u - \sum c_i B_i \right\|_H$$





# Linear Elasticity

displacement:

$$(u_1, u_2, u_3) \in (H_{\Gamma}^1)^3$$

strain tensor:

$$\varepsilon_{k,l} = \frac{1}{2} (\partial_k u_l + \partial_l u_k)$$

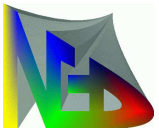
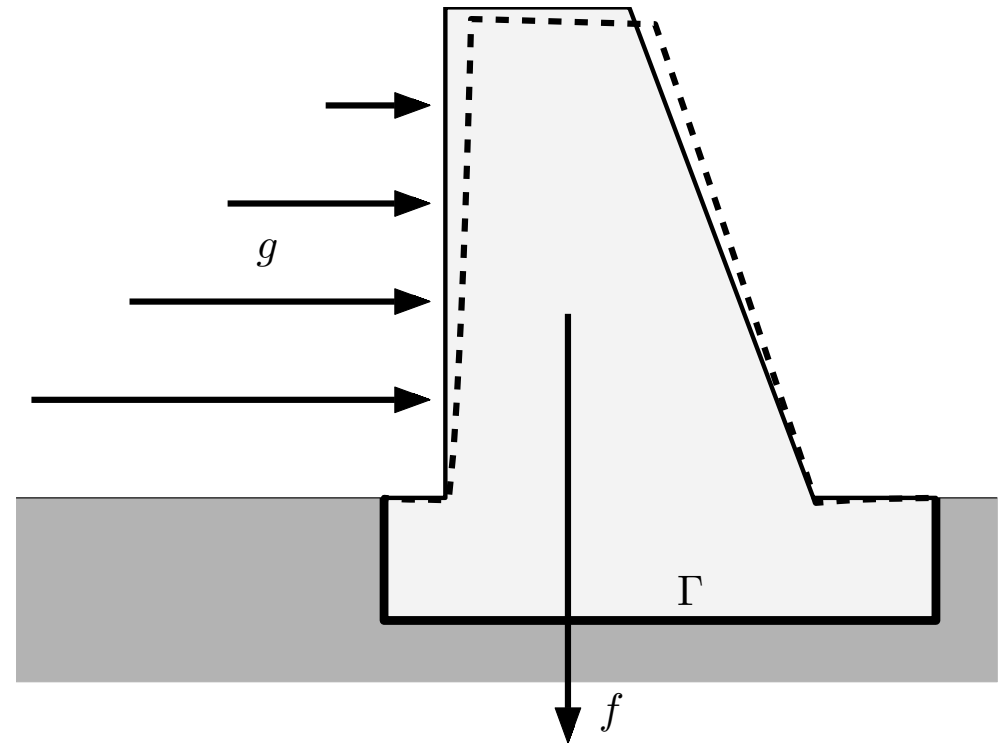
stress tensor;

$$\sigma_{k,l} = \lambda(\text{trace } \varepsilon)\delta_{k,l} + 2\mu\varepsilon$$

variational formulation:

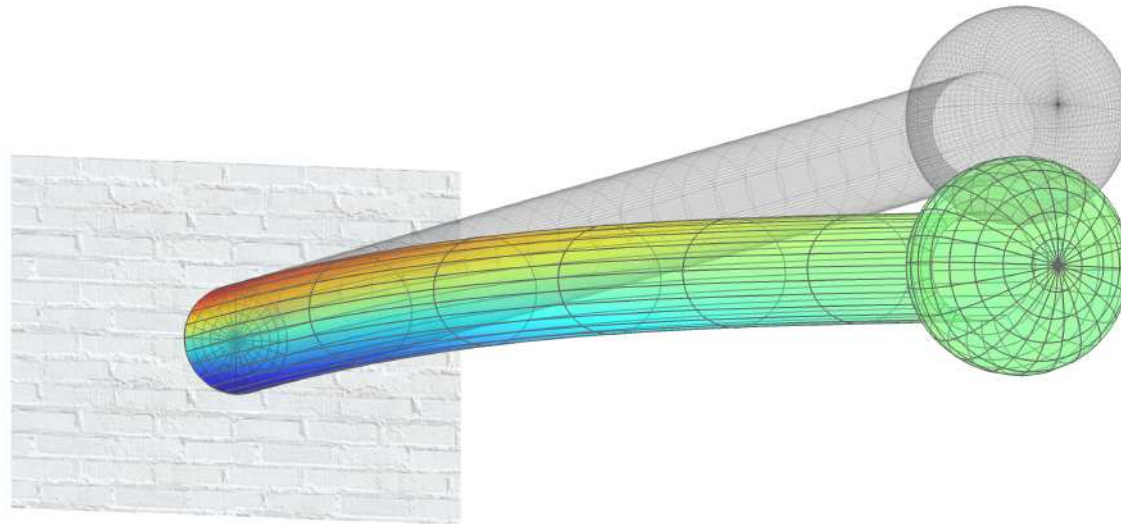
$$a(u, v) = \int_{\mathcal{D}} \sigma : \varepsilon$$

$$\lambda(v) = \int_{\mathcal{D}} f v + \int_{\partial\mathcal{D} \setminus \Gamma} g v$$

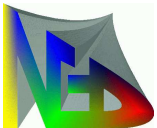


# Flagstaff

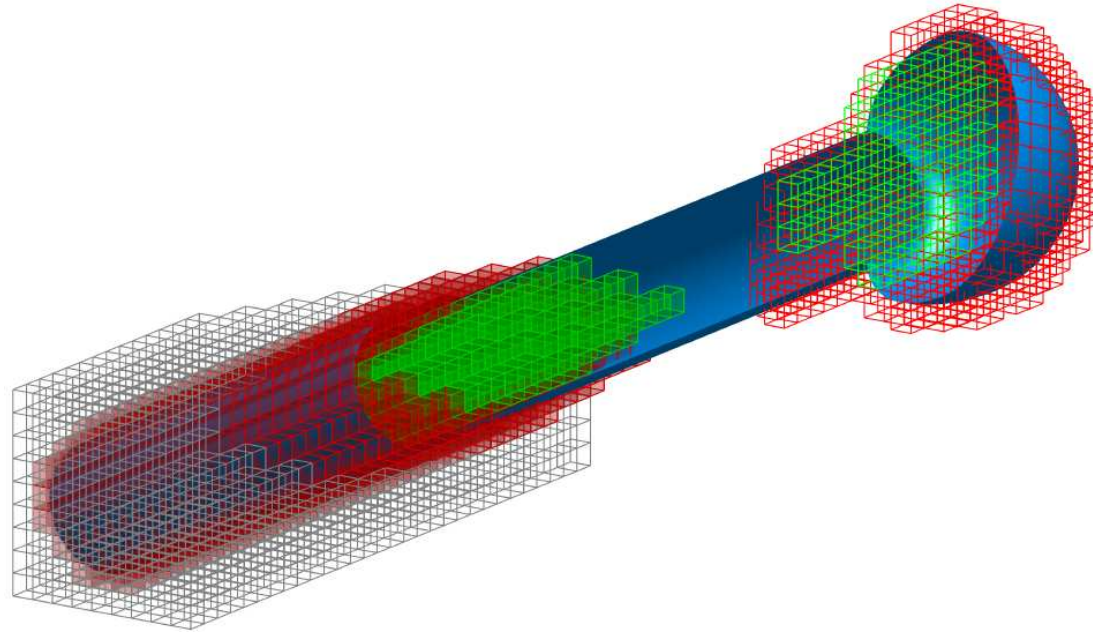
displacement (30x) and principle stress (color)



rod length:	4.0m	head diameter:	0.4m
material:	aluminum	$\lambda$ :	$5.71 \cdot 10^8 \text{N/dm}^2$
		$\mu$ :	$2.69 \cdot 10^8 \text{N/dm}^2$
max displacement:	9mm	max stress:	1.7kN/cm <sup>2</sup>

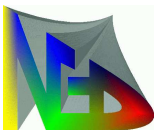


# Flagstaff



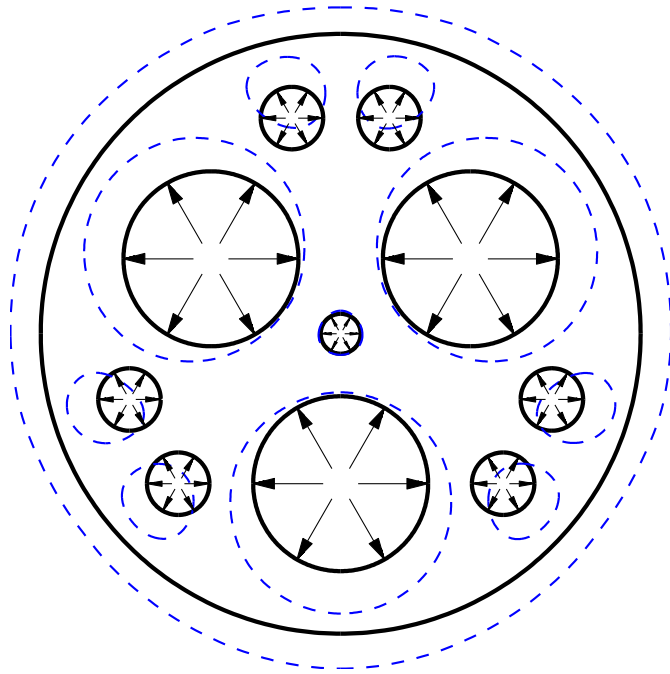
grid cell classification

grid width	0.9	0.45	0.225	0.1125
inner	56	1036	10506	101606
boundary	450	1794	7242	31862
ratio	0.889	0.634	0.408	0.239

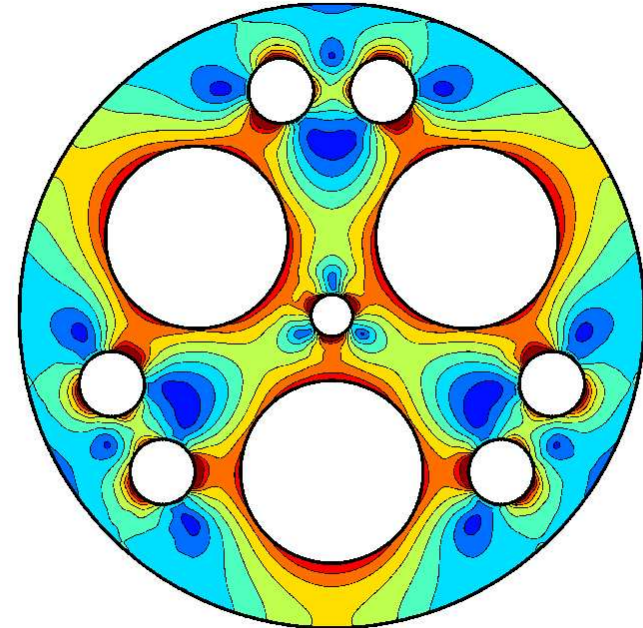


# Plane Strain

$$\varepsilon_{3,l} = \varepsilon_{l,3} = 0$$

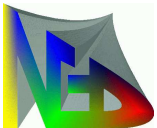


displacement

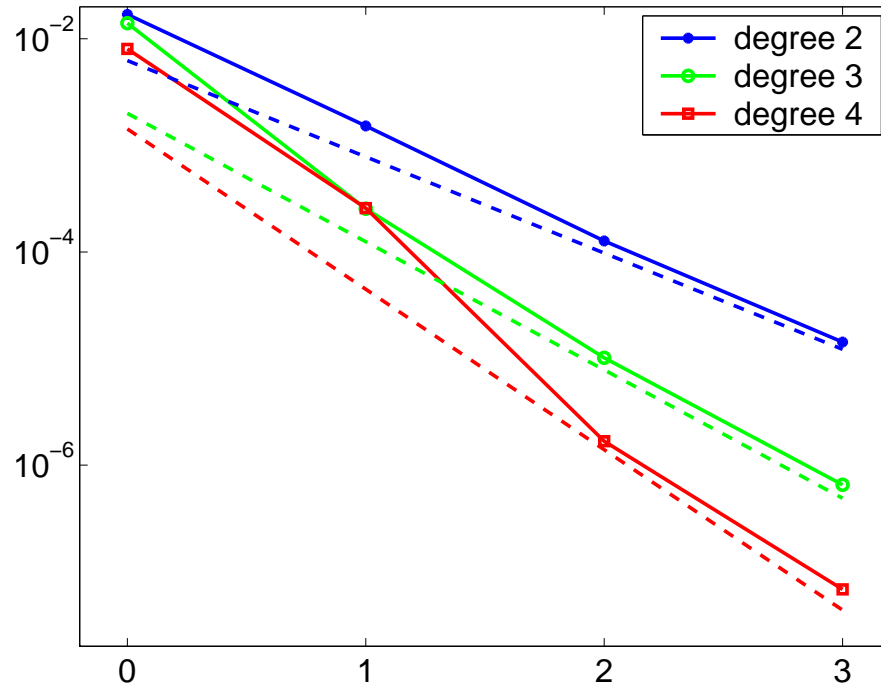


principal stress

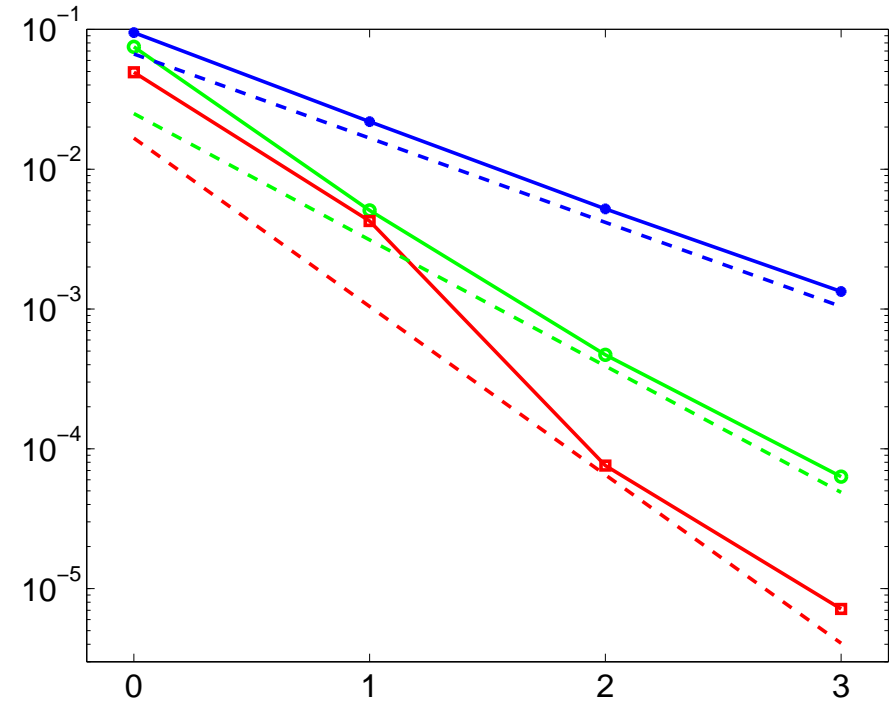
same pressure ( $40 \text{ kp/cm}^2$ ) in all pipes, no force on outer boundary  
material steel:  $\lambda = 1.15\text{e}7 \text{ N/cm}^2$ ,  $\mu = 7.7\text{e}6 \text{ N/cm}^2$   
outer circle:  $r_o = 120\text{cm}$



# $L^2$ - and $H^1$ -Error

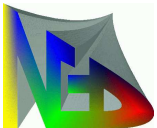


$$\|u - u_h\|_0 \leq h^{n+1}$$

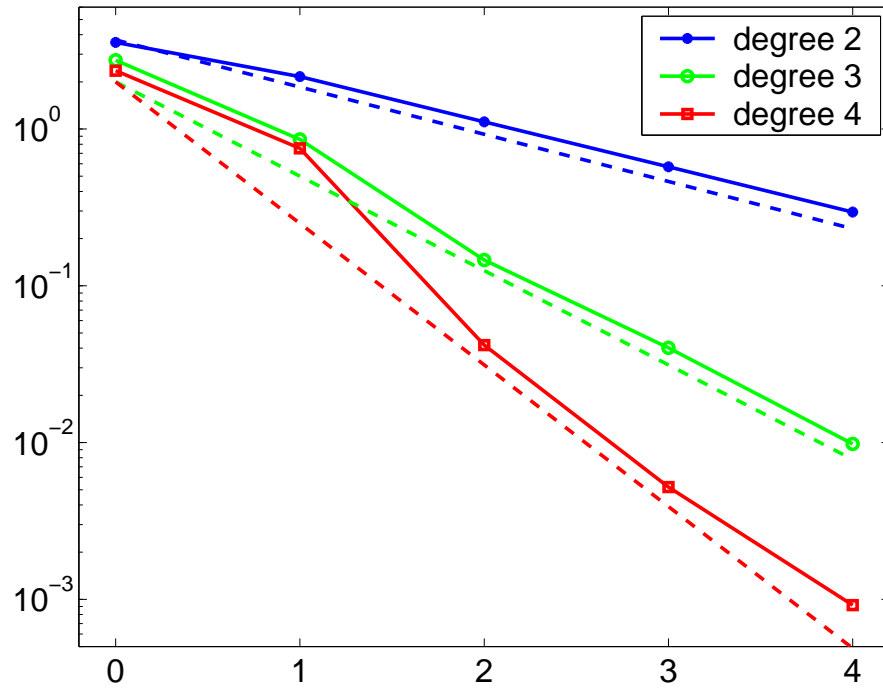


$$\|u - u_h\|_1 \leq h^n$$

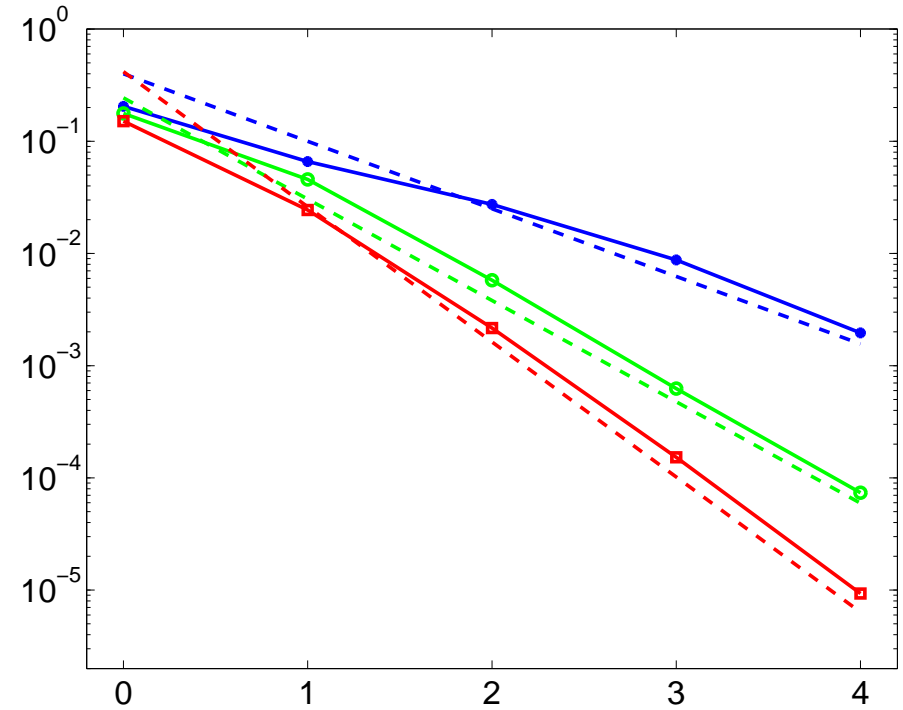
$$h = 2^{-k} h_0, \quad 84 \dots 4752 \text{ basis functions}$$



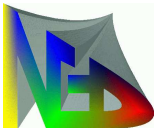
# Residuum and Boundary Error



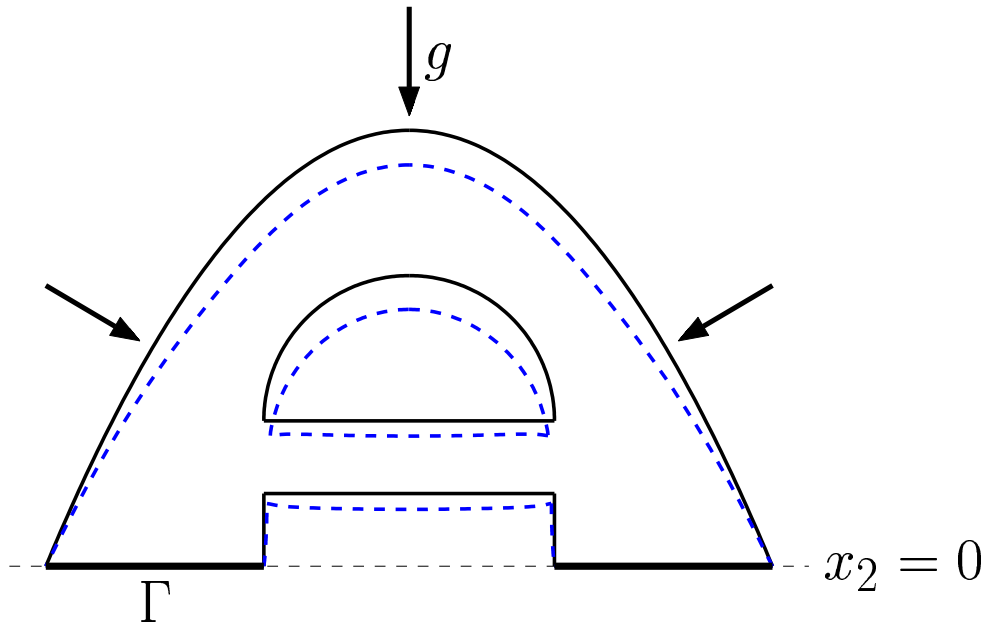
$$\|\operatorname{div} \sigma + f\|_0 \preceq h^{n-1}$$



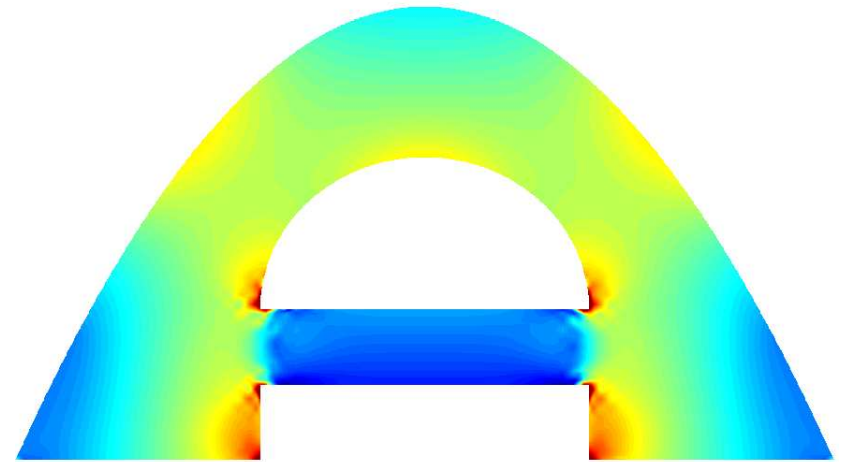
$$\max_{\partial D \setminus \Gamma} |\sigma \xi - g| \preceq h^n$$



# Singular Solution

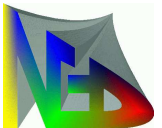


displacement



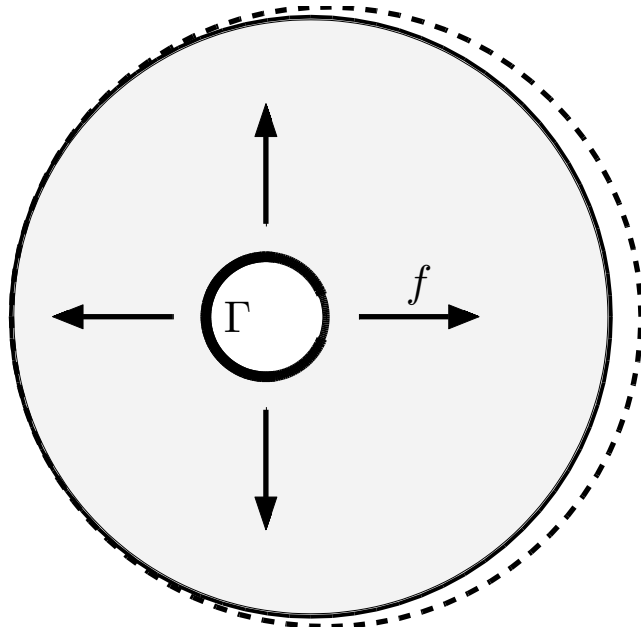
principal stress

material concrete:  $\lambda = 8.3e9 \text{ N/m}^2$ ,  $\mu = 1.25e10 \text{ N/m}^2$

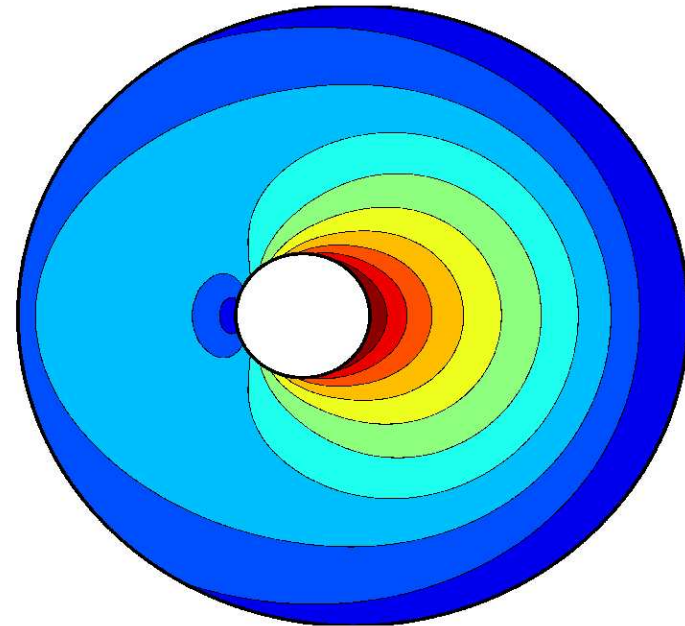


# Plane Stress

$$\sigma_{3,l} = \sigma_{l,3} = 0$$

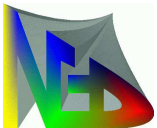


displacement



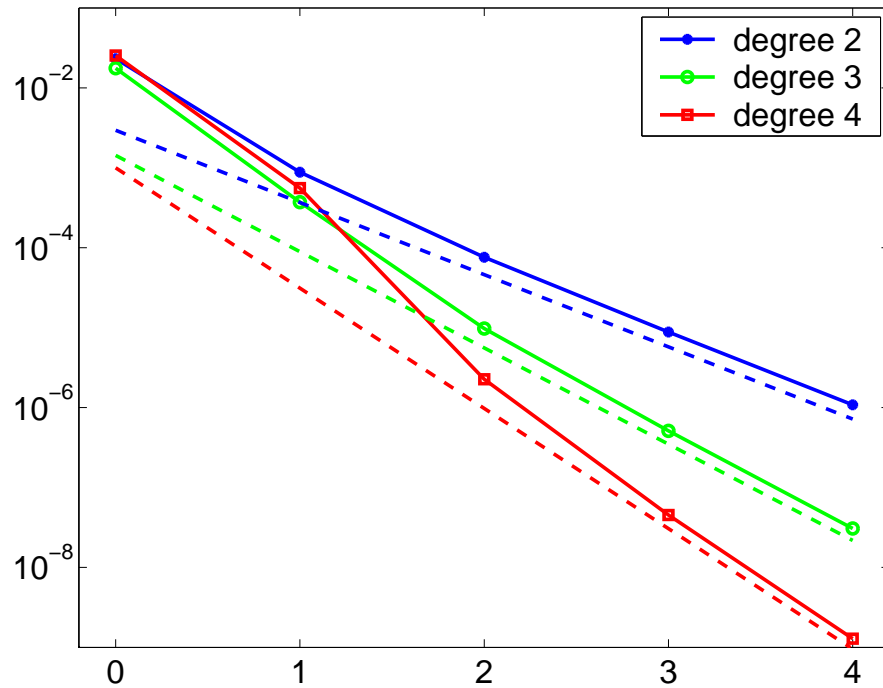
principal stress

material steel:  $\lambda = 1.05e7 \text{ N/cm}^2$ ,  $\mu = 8.28e6 \text{ N/cm}^2$   
volume force  $f = 10^4(x, y)^t \text{ N/cm}^3$   
outer circle:  $r_o = 5\text{cm}$ ,  $M_o = (3/4, 0)$   
inner circle:  $r_i = 1\text{cm}$ ,  $M_i = (0, 0)$

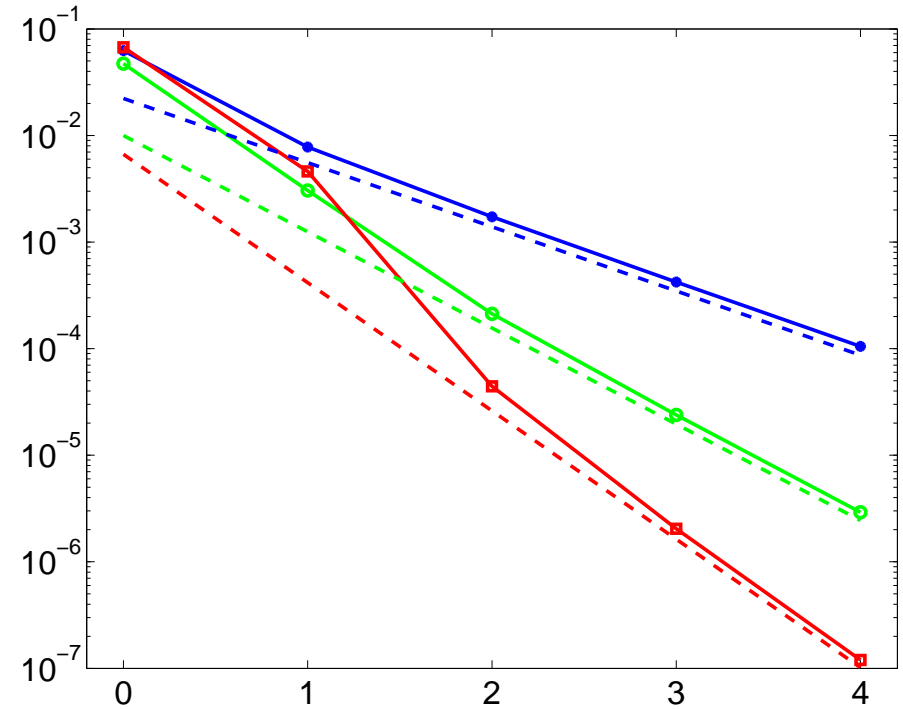




# $L^2$ - and $H^1$ -Error

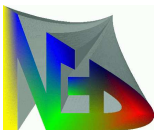


$$\|u - u_h\|_0 \preceq h^{n+1}$$

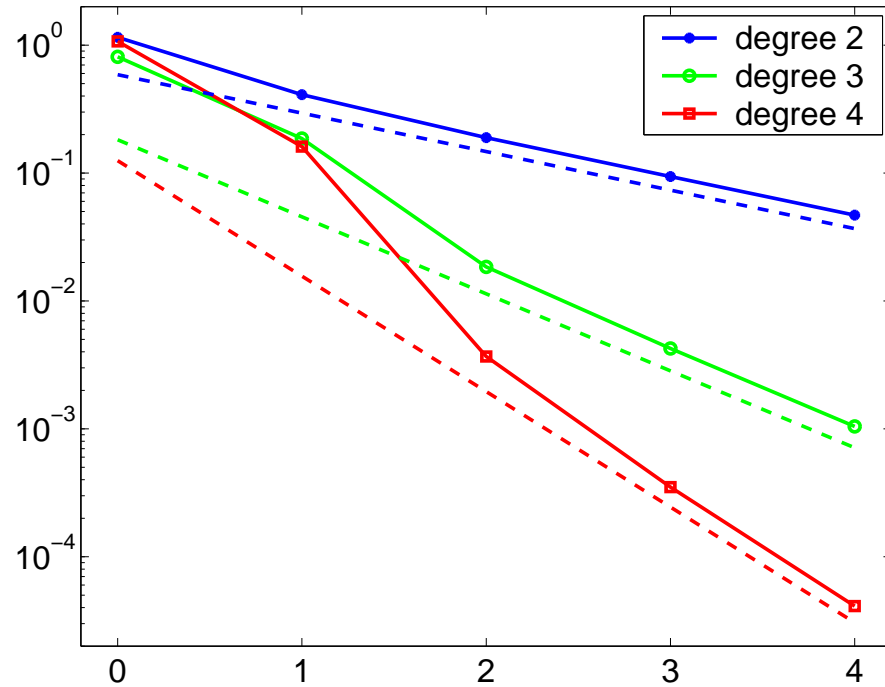


$$\|u - u_h\|_1 \preceq h^n$$

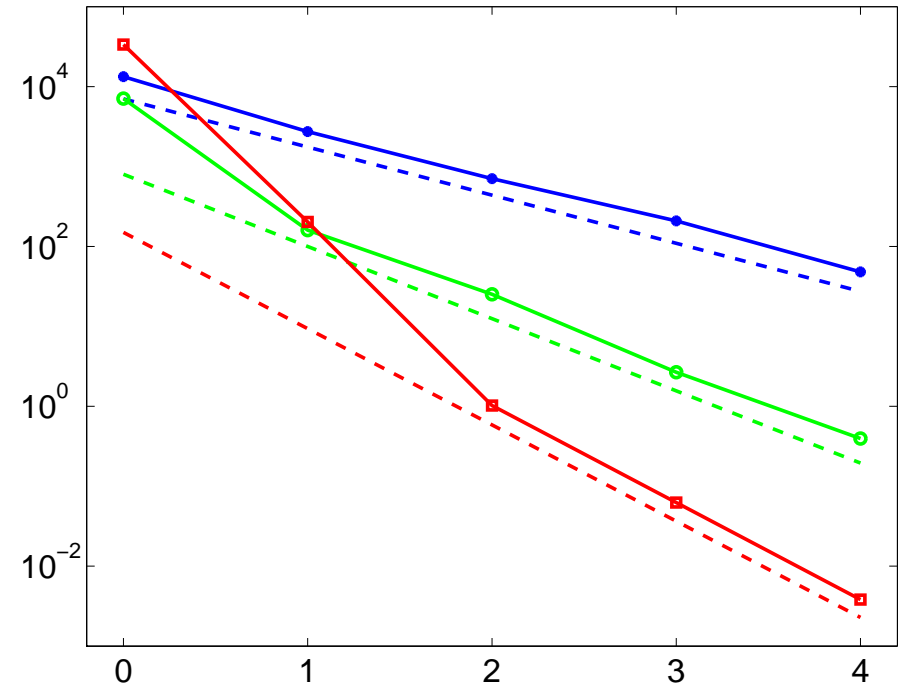
$$h = 2^{-k} h_0, \quad 196 \dots 40896 \text{ basis functions}$$



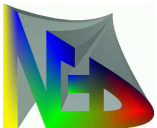
# Residuum and Boundary Error



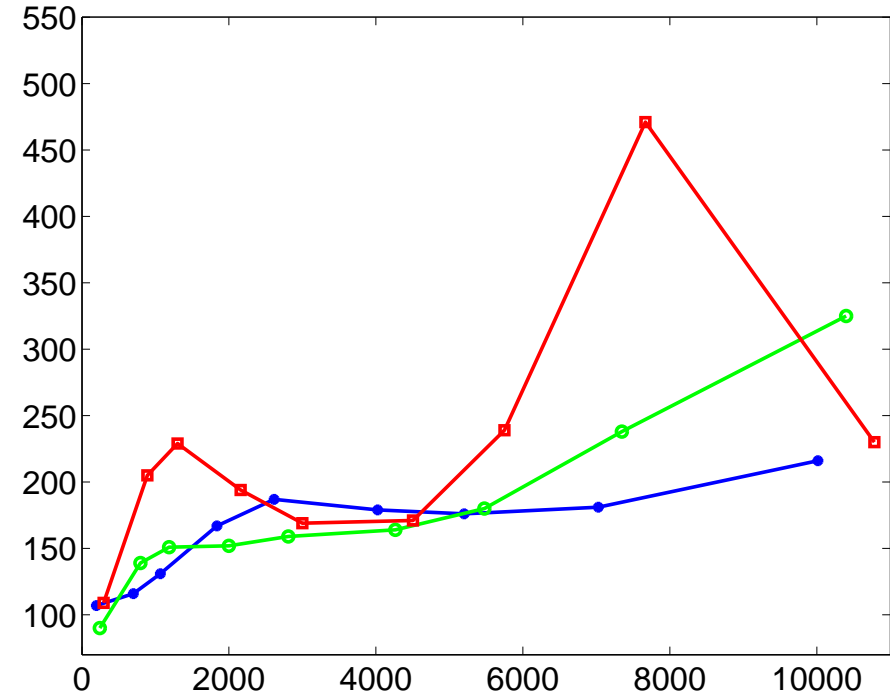
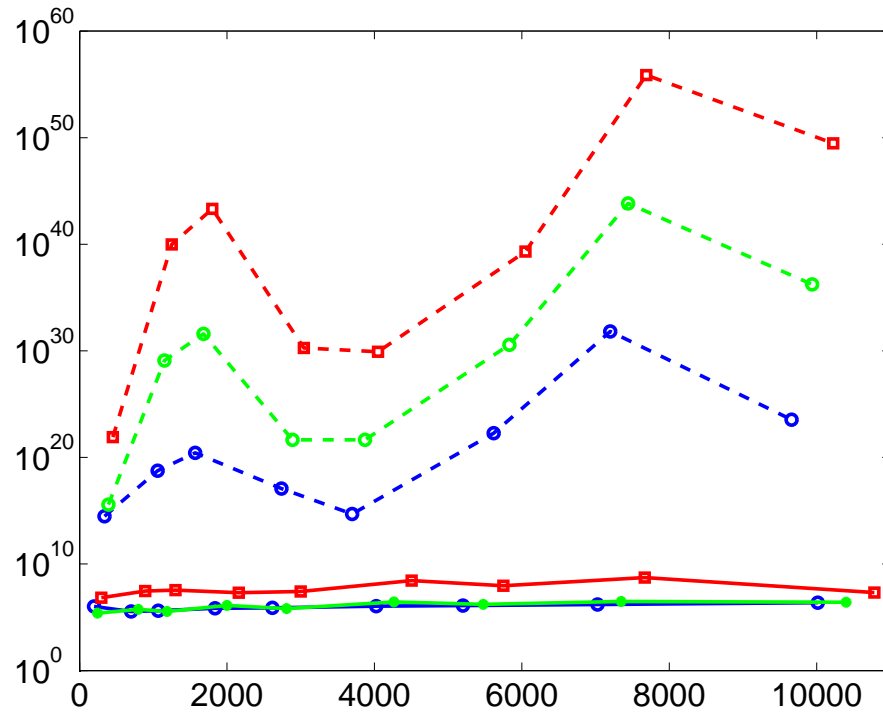
$$\|\operatorname{div}\sigma + f\|_0 \preceq h^{n-1}$$



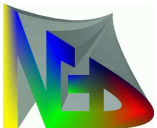
$$\max_{\partial D \setminus \Gamma} |\sigma\xi - g| \preceq h^n$$



# Condition Number and Iteration Count



$$\text{cond}(G_h) \sim h^{-2} \sim \text{dim}^{-1}$$



# Advantages of web-Splines

- no mesh generation
- simple basis functions
- multigrid techniques
- high accuracy with few parameters
- arbitrary smoothness and approximation order
- hierarchical bases

